

SCAL, Inc.

SPECIAL CORE ANALYSIS LABORATORIES

University Lands
Surface & Mineral Interests
P. O. Box 553
Midland, TX 79702

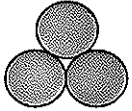
Cimarex Energy Company of Colorado

Sidewall Core Analysis Report

University 18-41 "A" No. 1-H Ward County, Texas

The analysis, interpretations or opinions expressed in our reports represent the best judgement of Special Core Analysis Laboratories Inc.. Special Core Analysis Laboratories Inc. assumes no responsibility and makes no warranties of any kind as to the productivity, proper operation or profitability of any oil, gas, or any other mineral in connection which such a report is used or relied upon.

P.O. Box 9730 - MIDLAND, TX 79708-2730 - (432) 561-5406 - FAX (432) 561-5339



SCAL, Inc.

SPECIAL CORE ANALYSIS LABORATORIES

May 23, 2007

Ms. Taru Parvin

Cimarex Energy Company of Colorado
5215 N. O'Connor Blvd.
Suite 1500
Irving, Texas 75039

Reference: Drilled Sidewall Core Analysis
File: 07674
University 18-41 "A" No. 1-H
Ward County, Texas

Dear Ms. Parvin:

Please find enclosed the final core analysis report for the rotary sidewall core samples.

The following procedures were used:

The sample containers were opened and a gas detector was used to determine the presence and relative amount of flammable gas. The gas measurement of 500+ represents the point at which the gas detector filament becomes saturated. The ends of the samples were trimmed and UV and Natural light photographs were taken. The end piece of each sample was then photographed under natural light utilizing a microscope at a low (10x) and higher (30x) magnification. A Dean-Stark extraction was performed to remove the pore water. The remaining oil was extracted using a CO₂-Toluene core cleaner. A material balance was performed to determine the oil saturation. After drying, the porosity, air permeability (@ 500 psi and reservoir stress) and grain density were measured.

It was a pleasure performing these analysis for you. If you have any further questions please feel free to contact our laboratory.

Thank you for using SCAL, Inc.

Sincerely,

Landon Turnbow
Lab Supervisor

John Shuler
Lab Manager

Mihai Vasilache
Petroleum Engineer/President

U.T. LANDS

MAY 24 2007

WTO



SCAL, Inc.

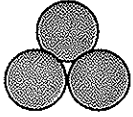
SPECIAL CORE ANALYSIS LABORATORIES

Rotary Sidewall Core Analysis Procedure, Results and Limitations

December 20, 2004

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Rotary Sidewall Core Analysis Procedure

1. Assigning sample numbers.

The sample numbers are assigned sequentially from top to bottom depth. A label with the sample number is applied to each sample jar.

2. Flammable gas detection.

The sidewall rotary cores arrive at the laboratory in glass jars. After inspecting the seal condition of the jars the gas evolved from the samples is measured using a multichannel digital system. SCAL, Inc. developed a new equipment and procedure allowing the gas evaluation without further gas dilution. The gas detector is calibrated using 1% methane in air as 100 gas units.

The gas readings are used to determine if gas hydrocarbons are present in a given sample. Before one makes a judgement on the existence of gas hydrocarbons there are several factors that need serious consideration:

Mud gas contamination. If the well has a open hydrocarbon zone it is very likely that gas and liquid hydrocarbons are present in the entire mud system. By looking at all the gas readings most of the time it is possible to establish some background gas level. Samples showing gas readings higher than the background are likely gas sources, where samples with values close to the background probably are contaminated.

The process used to cut and recover the cores has serious effects on the gas readings. The sidewall cores are invaded by mud filtrate during the coring process. If the sampled formation has permeability and hydrocarbons, the filtrate invasion will displace the hydrocarbons to saturations close to the residual level. As the cores are lifted from the formation pressure and temperature to surface conditions of pressure and temperature the gas will come out of solution and expand. This gas expansion will unload some of the fluids present in the pore space. The time elapsed from the cutting of the core to the time it is sealed in the glass jar is important. A long sample unloading, examination and description combined with good sample permeability and strong fluid invasion can yield low gas readings.

3. Sample trimming and marking.

The end pieces are trimmed in order to obtain a right cylindrical core. A diamond blade cooled with water is used if the cores were drilled with a water based mud. Other fluids are available for special cases (i.e. oil based drilling muds). The larger the core samples the more accurate the laboratory measurements will be. Ask the coring company to install a "long barrel" and cut the longest sidewall cores they can. This is a very important detail. The samples and end pieces are marked with a sample number.

4. Fluorescence evaluation.

The samples fluorescence is graded on a 0 to 100% scale and described with respect to intensity, color, distribution and cut.

5. Digital sample photography.

Each sample is photographed in daylight and ultraviolet. A centimeter scale is used in the photo setup allowing sample size evaluation. We then photograph the end pieces using a composite format (12 samples in the same frame) to provide the ability to compare the fluorescent colors and intensity independent of photo processing,

6. The original weight of the sample is electronically measured and recorded and the samples are loaded in individual Dean-Stark extractors to clean the samples and measure the fluid content for assessing the water and oil saturations. The water extracted is recorded at the end of the extraction process.

If the samples are tight and the Dean-Stark extraction process was not complete the samples are loaded in a digitally controlled plug toluene-CO₂ cleaner and the extraction process is continued until all hydrocarbons are removed.

If salt crystals are present within the pore system a long methanol Soxhlet extraction using methanol is recommended. Formations with high salinity water drilled with saturated brine are the most likely candidates for this additional step.

7. After extraction the cores are dried at 100 degrees C until the weight of the sample becomes constant. special drying procedures are available for special samples containing gypsum, clays or other temperature sensitive minerals. These methods include low temperature and controlled humidity drying.

8. The samples are cooled in an automated desiccator and the dry weight of the samples is measured and recorded electronically.

9. The sample's dimensions are measured and recorded using digital precision calipers interfaced in the computer system.

10. The samples are loaded into automated He expansion equipments and the grain volumes are measured.

11. If the desired confining pressure is not specified SCAL, Inc. will average the depths for each zone and will estimate the net uniaxial overburden stress assuming 1 psi/ft weight of the overburden, normal pressurized reservoir and average Poisson ratio.

12. The samples are loaded into an automated Klinkenberg system at 500 psi confining pressure (required for a good seal). After equilibrium a helium expansion porosity is conducted followed by a Klinkenberg permeability measurement. The reference volume and the sample is filled with helium and after equilibrium the helium is produced recording pressure-time data. The system integrates the data determining the Klinkenberg permeability (a liquid permeability to a non reactive liquid).

13. The porosity and Klinkenberg permeability are performed at the reservoir stress as determined in 11.

Small sample size, imperfect cylinder and drilling induced fractures are the most common problems yielding inaccurate core analysis measurements. When a porosity is too good to be true it is probably due to the sample shape and size. The very high permeability (out of context) is sometimes due to a drilling induced fracture. However the confining stress measurements reduce these errors. The relaxed fractures tend to close at reservoir stress.

The most realistic data will be the Klinkenberg permeability and porosity determined at reservoir stress. The "ambient" (500 psi) is provided to compare the subject cores with old core analysis measured by the old technology.

14. The fluid saturations are calculated. The recorded Dean-Stark water divided by the pore volume represents the water saturation. To calculate the oil saturation a material balance is performed. The original weight minus the dry weight minus the water recovered represents the oil extracted from the sample.

The water and oil saturations are affected by several factors; mud filtrate invasion during the coring, gas expansion during core retrieval to surface, sample handling in the field and laboratory, sample size and its porosity. A small tight sample with low porosity can have a very small pore volume making the saturation calculation inaccurate or even impossible.

A very high water saturation without fluorescence and without significant (higher than the background gas) gas units will indicate a wet zone, where moderate water saturations with some gas units will indicate "gas expansion" in the core retrieval process therefore a "gas zone". Oil fluorescence associated with some oil saturations (e.g. the residual range due to invasion) will indicate an "oil zone".

The gas readings and fluid saturations are subject to fluid invasion, gas expansion, drilling parameters and field handling.

15. A geological sample description along with low and high magnification stereo microscope photos is done. The core end pieces are mounted in coin holders, labeled with the depth and included in the final report.

16. The final core analysis report is prepared as paper and digital versions. Plots of permeability versus porosity and the reservoir quality index versus normalized porosity are included. All digital pictures are printed and copied to the CD and can be used as desired by the client and its partners.

SCAL, Inc. is equipped with state-of-the-art technology; it maintains qualified and experienced laboratory personnel, and uses multiple sets of hi-tech automated equipment for each step of this procedure to provide this type of analysis on a fast turnaround basis making it possible for our clients to make a pipe setting decision on reservoir stress core analysis data.

We will be happy to work with you and modify this "standard" procedure to meet your specific needs. Thank you for considering SCAL, Inc.

Sincerely,

A handwritten signature in black ink, appearing to read "Mihai Vasilache", with a long horizontal flourish extending to the right.

Mihai A. Vasilache
Petroleum Engineer, President

Drilled Sidewall Core Analysis Report

Company: Cimarex Energy Company of Colorado
File No.: 07674
Well : University 18-41 "A" No. 1-H
Location: 680' FSL & 680' FWL, Sect. 41, Blk 18, University Lands Survey
Field: War Wink, W.
Formation: Wolfcamp
County: Ward County, Texas

Sample Number	Depth ft	Air Permeability		Klinkenberg Permeability		Porosity %	Grain Density g/cc	Sw %	So %	Gas Units	Fluorescence		Sample Description
		mD	mD	mD	mD						%	Description	

Confining Pressure 3,775psi

1	11,316.0	0.0398	0.0216	10.60	2.68	49.1	17.3	345	100	Yl-gm	Ss:tn xfg wl srt md v sl dol
2	11,318.0	0.0493	0.0288	9.94	2.66	42.3	17.7	297	100	Yl-gm	Ss:tn xfg wl srt md v sl dol v sl pyr
3	11,320.0	0.0633	0.0392	10.29	2.64	39.4	18.1	355	100	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr
4	11,327.0	0.0373	0.0205	10.38	2.66	46.6	16.8	304	90	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr sl sh
5	11,337.0	0.0093	0.0035	7.94	2.68	74.1	0.0	345	tr	Yl-gm	Silty/Sh:brm intrgr por v sl sd sm dol sm pyr
6	11,339.0	0.0333	0.0183	8.26	2.66	47.0	17.5	260	100	Yl-gm	Ss:tn vfg wl srt md v sl dol
7	11,340.0	0.0362	0.0201	8.59	2.67	44.0	18.6	500+	100	Yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr
8	11,353.0	0.0658	0.0409	10.76	2.66	42.2	18.2	500+	100	Yl-gm	Ss:tn vfg wl srt md sm dol sl pyr
9	11,355.0	0.0680	0.0420	11.08	2.65	45.3	18.9	500+	100	Yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr
10	11,357.0	0.0942	0.0620	11.31	2.65	40.8	18.5	500+	100	Yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr
11	11,359.0	0.0788	0.0507	10.99	2.65	43.4	19.1	500+	100	Yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr
12	11,361.0	0.0611	0.0368	10.20	2.67	44.2	19.9	456	100	Yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr
13	11,363.0	0.0169	0.0081	7.41	2.79	69.3	0.0	500+	0	Yl-gm	Silty/Sh:sm intrgr por v sl sd v sl dol pyr
14	11,381.0	0.0011	0.0002	4.11	2.72	64.1	0.0	500+	tr	Yl-gm	Ss:brn xfg wl srt md calc v sl pyr v sl sh
15	11,390.0	0.0190	0.0094	6.88	2.67	71.8	0.0	470	tr	Yl-gm	Siltst:brn xfg wl srt md sl dol v sl pyr v sl sh
16	11,406.0	0.0150	0.0066	7.11	2.71	45.5	17.1	500+	90	Di yl-gm	Ss:tlbrn vfg wl srt md sm calc v sl pyr v sl sh
17	11,419.0	0.0118	0.0040	6.88	2.72	70.1	0.0	500+	tr	Di yl-gm	Siltst:drkbrn xfg wl srt md sl sd v sl dol v sl pyr
18	11,421.0	0.0566	0.0337	11.04	2.69	43.6	19.5	500+	100	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr
19	11,423.0	0.0281	0.0144	8.98	2.76	41.8	17.2	500+	100	Yl-gm	Ss:tn vfg wl srt md sm calc v sl pyr
20	11,425.0	0.1213	0.0829	12.57	2.68	44.6	17.8	500+	100	Yl-gm	Ss:tn vfg wl srt md v sl pyr

Drilled Sidewall Core Analysis Report

Company: Cimarex Energy Company of Colorado **Field:** War Wink, W.
File No.: 07674 **Formation:** Wolfcamp
Well : University 18-41 "A" No. 1-H **County:** Ward County, Texas
Location: 680' FSL & 680' FWL, Sect. 41, Blk 18, University Lands Survey

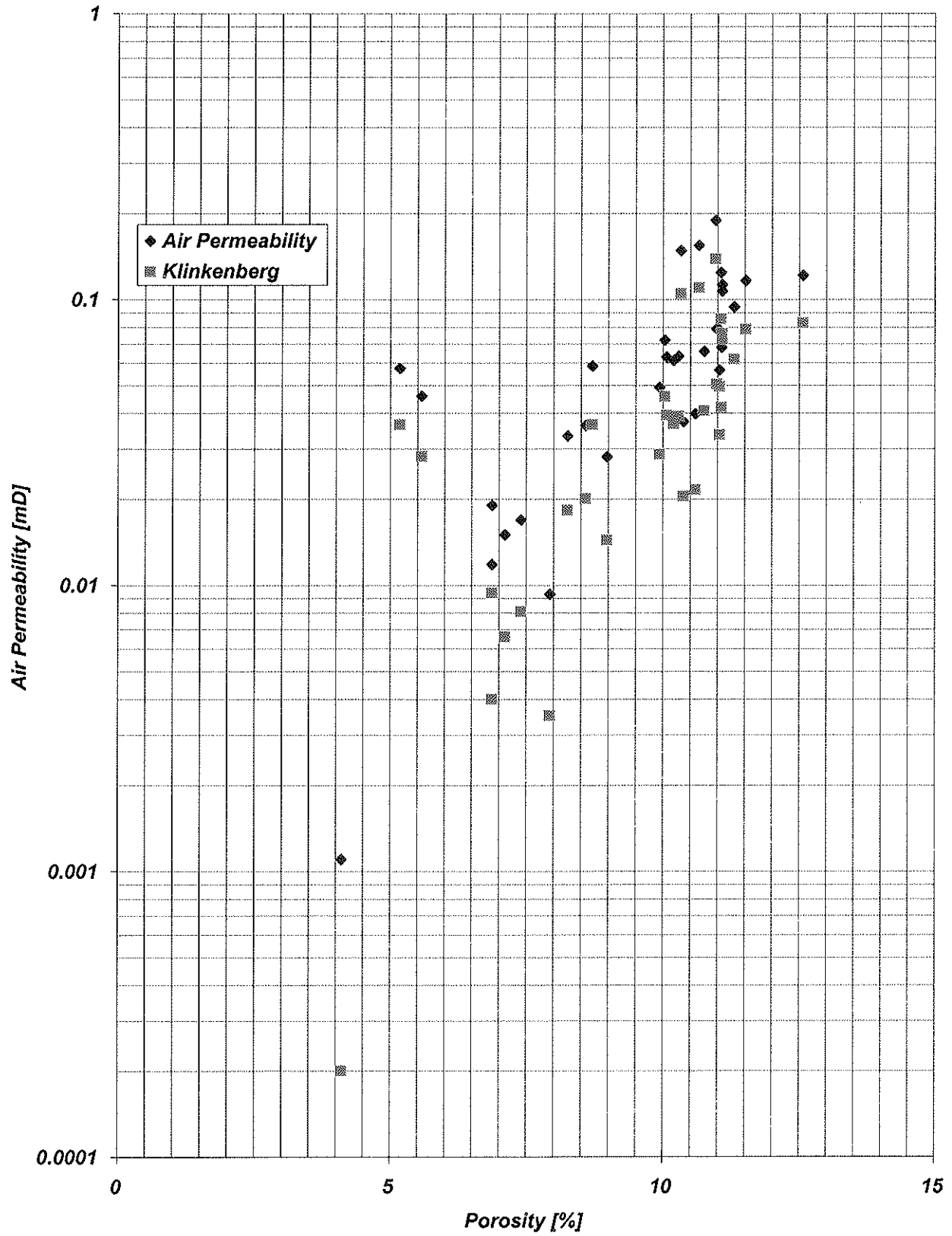
Sample Number	Depth ft	Air		Klinkenberg		Porosity		Grain		Sw	So	Gas	Fluorescence		Sample Description
		Permeability mD	Permeability mD	Permeability mD	Density g/cc	%	%	Units	%				Description		
21	11,431.0	0.0781	0.0496	0.0496	2.70	11.04	46.9	19.4	476	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr	
22	11,433.0	0.1243	0.0856	0.0856	2.69	11.07	43.0	17.4	500+	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md v sl dol sl pyr	
23	11,435.0	0.1127	0.0761	0.0761	2.69	11.09	41.6	19.3	500+	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr	
24	11,437.0	0.0629	0.0394	0.0394	2.72	10.07	40.1	19.0	500+	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md sl dol v sl pyr	
25	11,439.0	0.0721	0.0458	0.0458	2.71	10.04	44.7	17.6	500+	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md sl dol v sl pyr	
26	11,440.5	0.1165	0.0788	0.0788	2.69	11.52	39.8	18.9	500+	100	Yl-gm	100	Yl-gm	Ss:tn vfg wl srt md v sl dol v sl pyr	
27	11,452.0	0.0585	0.0366	0.0366	2.70	8.71	66.0	0.0	500+	tr	Yl-gm	tr	Yl-gm	Silty/Ss:xf-vfg mod srt md sl dol sm pyr	
28	11,473.0	0.0459	0.0283	0.0283	2.66	5.58	70.8	0.0	500+	tr	Yl-gm	tr	Yl-gm	Siltst:bm xfg wl srt md sm dol v sl pyr	
29	11,495.0	0.0574	0.0366	0.0366	2.72	5.18	62.4	0.0	500+	tr	Yl-gm	tr	Yl-gm	Siltst:bm xfg wl srt md sm sd sm dol sm pyr	
30	11,516.0	0.1481	0.1052	0.1052	2.69	10.33	38.8	19.7	500+	100	V dl yl-gm	100	V dl yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr	
31	11,519.0	0.1890	0.1390	0.1390	2.69	10.97	41.3	18.0	489	100	V dl yl-gm	100	V dl yl-gm	Ss:tn vfg wl srt md sm dol	
32	11,521.0	0.1544	0.1103	0.1103	2.69	10.66	45.1	19.2	500+	100	V dl yl-gm	100	V dl yl-gm	Ss:tn vfg wl srt md sm dol v sl pyr	
33	11,523.0	0.1071	0.0729	0.0729	2.68	11.09	46.5	18.4	500+	100	Brt yl-gm	100	Brt yl-gm	Ss:tn vfg wl srt md sm dol	

Note: 500+ gas reading represents a saturated detector filament
 1% CH4 in air = 100 gas units

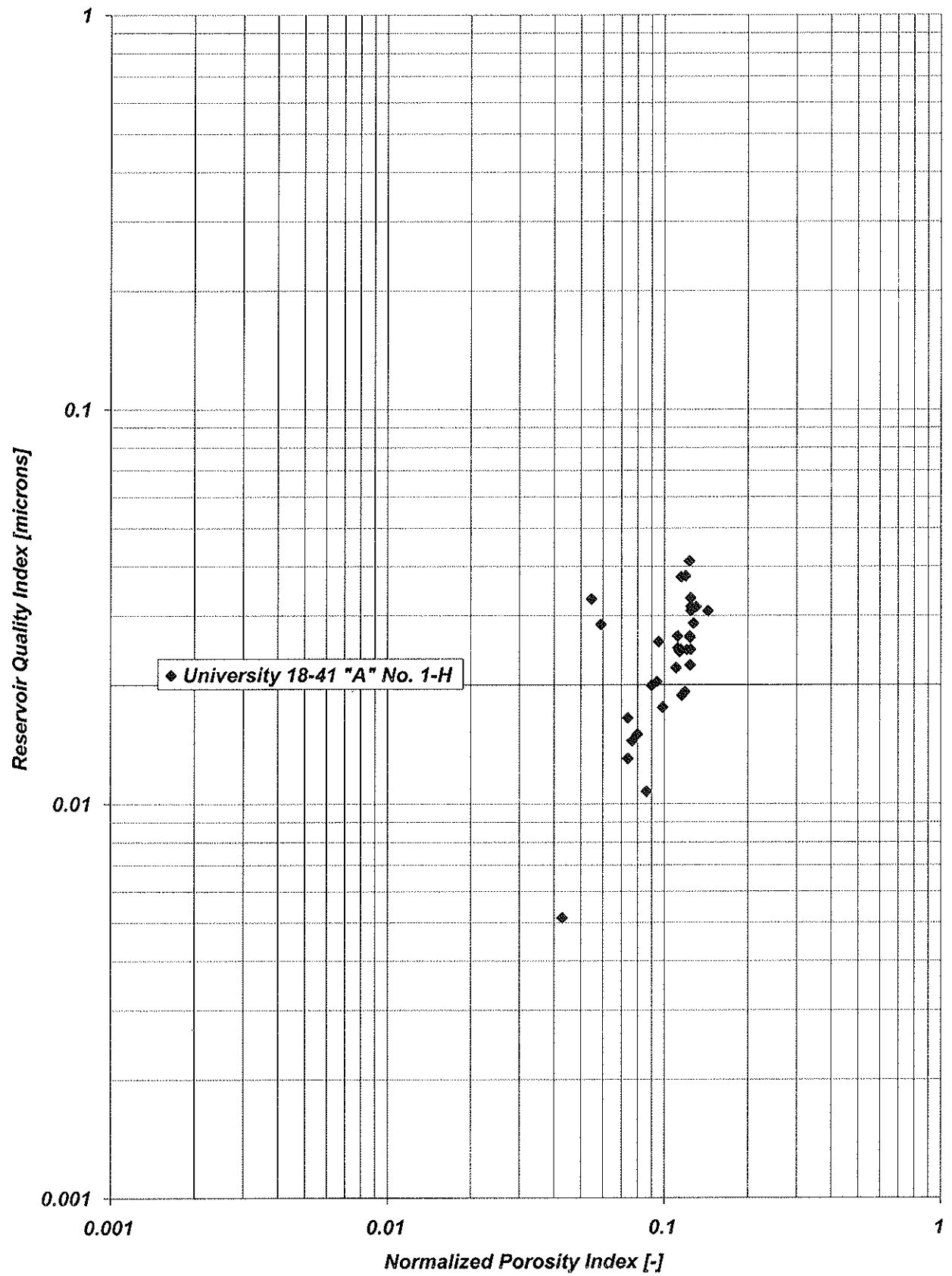
Core Description Abbreviations

ang	angular	gm	green	sbang	subangular
anhy	anhydrite	grst	grainstone	sc	surface contamination
ark	arkosic	gry	gray	sh	shale
arg	argillaceous	gyp	gypsum	strgr	stringer
bl	blue	h/frac	horizontally fractured	sbrnd	subround
bdgg	bleeding gas	hal	halite	scat	scattered
bdgo	bleeding oil	incl	inclusion	sd(y)	sand(y)
blk	black	intrgr	intergranular	sh	shale
blky	blocky	intrxin	intercrystalline	shy	shaley
brn	brown	ip	in part	sil	siliceous
brt	bright	lam	lamina(-ated)	sl	slight(ly)
bf	buff	ls	limestone	sily	silty
calc	calcareous	lt	light	sm	some
carb	carbonaceous	md	medium	sml	small
cem	cement	mf	mineral fluorescence	sp	spotty
cg	coarse grain	mg	medium grain	ss	sandstone
cgl	conglomerate	micr	micritic	silst	siltstone
chky	chalky	mod	moderate	srt	sorted
chty	cherty	mott	mottled	strks	streaks
com	common	mdst	mudstone	styl	stylolite
conch	conchoidal	n/a	not available	suc	sucrosic
cnsl	consolidated	n/r	not recovered	tbfa	too broken for analysis
crm	cream	nod	nodules	tn	tan
csit	coarse siltstone	nvp	no visible porosity	tr	trace
dk	dark	o	oil	v	very
dns	dense	ool	oolitic	vis	visible
dol	dolomite	ormg	orange	vfrac	vertically fractured
dolic	dolomitic	peld	peloid	vfg	very fine grain
dru	drusy	pisol	pisolitic	vug	vug(gy)
dul	dull	pk	pink	w/	with
fg	fine grain	pkst	packstone	wht	white
fiss	fissile	por	porosity	wk(-ly)	weak(-ly)
foss	fossiliferous	poss	possible	wkst	wackestone
frac	fractured	ppp	pinpoint porosity	wl	well
fri	friable	pr(-ly)	poor(-ly)	xln	crystalline
gil	gilsonite	ptg	parting	xfg	extremely fine grained
glauc	glauconite	pyr	pyrite	xl	crystal
		rmd	round	yl	yellow

Permeability versus Porosity @ 3,775psi



Reservoir Quality Index versus Normalized Porosity



Drilled Sidewall Core Analysis Report

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Location : 680' FSL & 680' FWL, Sect. 41, Blk 18, University Lands Survey	

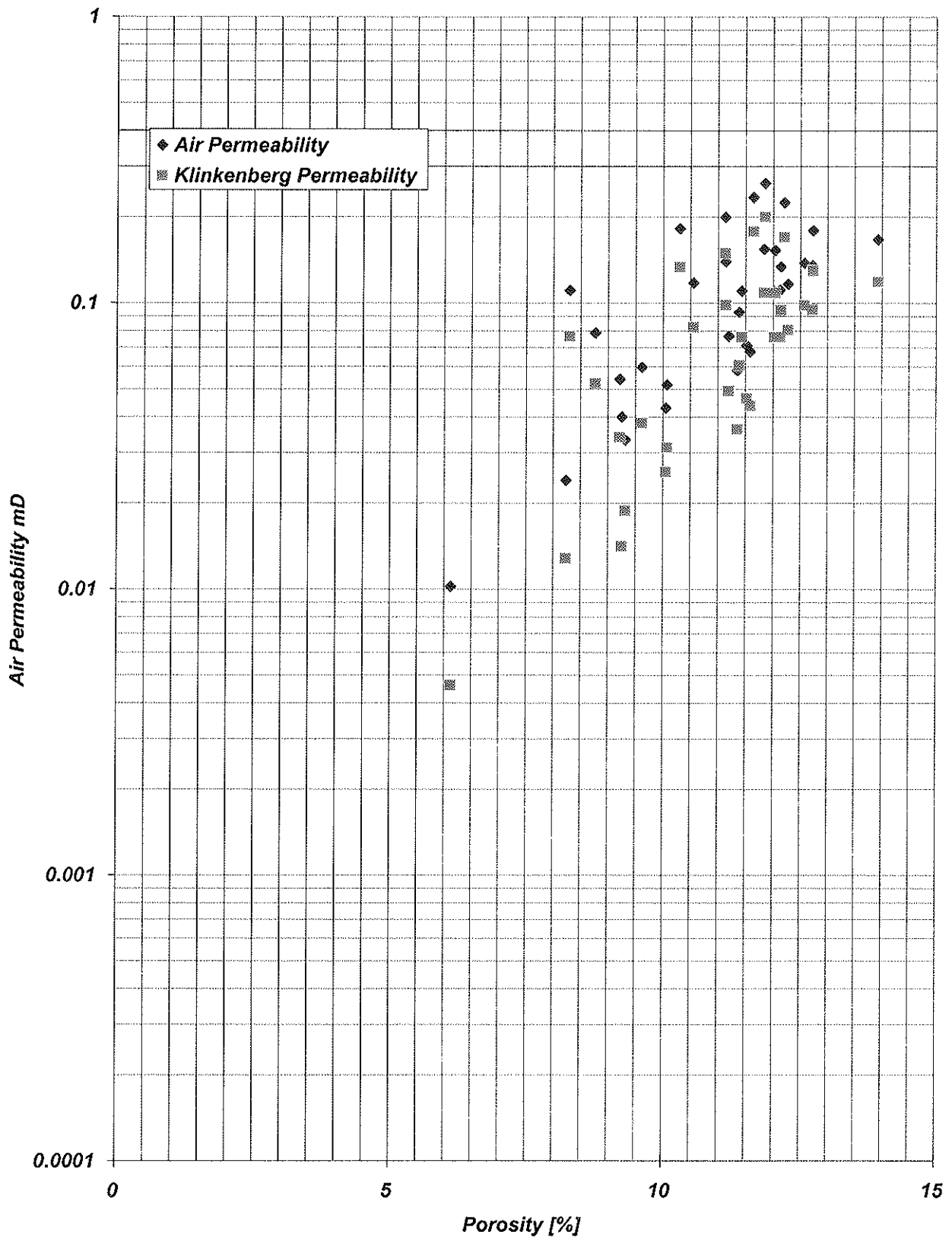
Sample Number	Depth ft	Grain Density g/cc	Porosity		Klinkenberg Permeability		Air		Porosity		Klinkenberg Permeability	
			%		mD		mD		%		mD	
Confining Pressure 500psi												
1	11,316.0	2.68	11.59		0.0675	0.0438		0.0398	10.60		0.0398	0.0216
2	11,318.0	2.66	11.36		0.0582	0.0362		0.0493	9.94		0.0493	0.0288
3	11,320.0	2.64	11.20		0.0766	0.0494		0.0633	10.29		0.0633	0.0392
4	11,327.0	2.66	11.53		0.0711	0.0465		0.0373	10.38		0.0373	0.0205
5	11,337.0	2.68	10.06		0.0429	0.0257		0.0093	7.94		0.0093	0.0035
6	11,339.0	2.66	9.22		0.0541	0.0340		0.0333	8.26		0.0333	0.0183
7	11,340.0	2.67	9.62		0.0596	0.0381		0.0362	8.59		0.0362	0.0201
8	11,353.0	2.66	12.03		0.1096	0.0761		0.0658	10.76		0.0658	0.0409
9	11,355.0	2.65	12.58		0.1377	0.0983		0.0680	11.08		0.0680	0.0420
10	11,357.0	2.65	12.73		0.1350	0.0948		0.0942	11.31		0.0942	0.0620
11	11,359.0	2.65	12.15		0.1338	0.0944		0.0788	10.99		0.0788	0.0507
12	11,361.0	2.67	11.39		0.0928	0.0606		0.0611	10.20		0.0611	0.0368
13	11,363.0	2.79	10.31		0.1817	0.1333		0.0169	7.41		0.0169	0.0081
14	11,381.0	2.72	6.13		0.0102	0.0046		0.0011	4.11		0.0011	0.0002
15	11,390.0	2.67	9.26		0.0399	0.0141		0.0190	6.88		0.0190	0.0094
16	11,406.0	2.71	8.24		0.0240	0.0128		0.0150	7.11		0.0150	0.0066
17	11,419.0	2.72	9.32		0.0332	0.0188		0.0118	6.88		0.0118	0.0040
18	11,421.0	2.69	12.28		0.1163	0.0806		0.0566	11.04		0.0566	0.0337
19	11,423.0	2.76	10.08		0.0517	0.0313		0.0281	8.98		0.0281	0.0144
20	11,425.0	2.68	13.93		0.1661	0.1185		0.1213	12.57		0.1213	0.0829

Drilled Sidewall Core Analysis Report

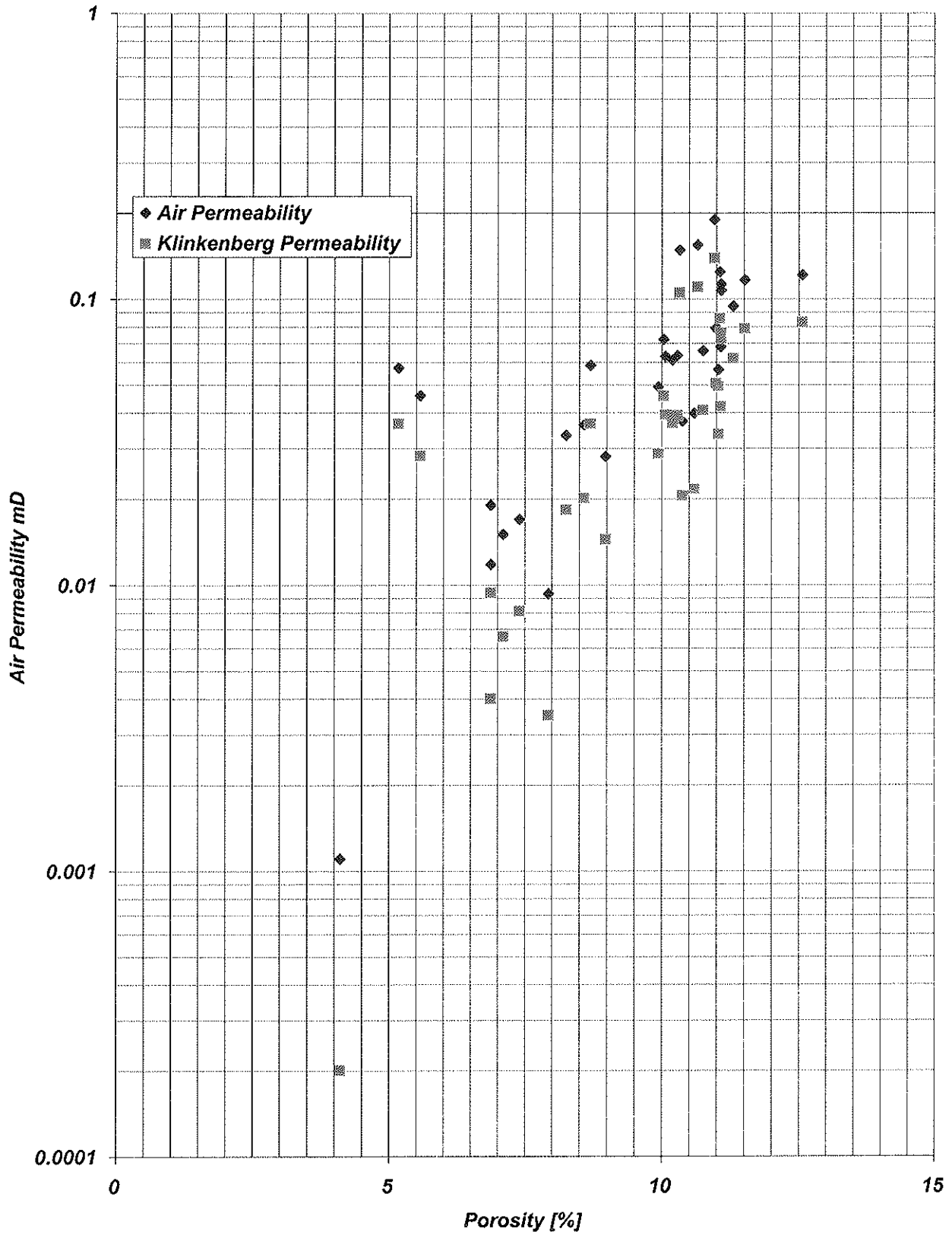
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Location : 680' FSL & 680' FWL, Sect. 41, Blk 18, University Lands Survey
Field: War Wink, W.
Formation: Wolfcamp
County : Ward County, Texas

Sample Number	Depth ft	Grain Density g/cc	Porosity		Klinkenberg		Air		Porosity		Air		Klinkenberg	
			%	%	Permeability mD	Permeability mD	Permeability mD	Permeability mD	%	%	Permeability mD	Permeability mD	Permeability mD	Permeability mD
Confining Pressure 500psi														
21	11,431.0	2.70	12.13	0.1110	0.0761	0.0781	0.0496	11.04	0.0781	0.0496	0.0781	0.0496	11.04	0.0781
22	11,433.0	2.69	11.84	0.1540	0.1089	0.1243	0.0856	11.07	0.1243	0.0856	0.1243	0.0856	11.07	0.1243
23	11,435.0	2.69	12.04	0.1525	0.1086	0.1127	0.0761	11.09	0.1127	0.0761	0.1127	0.0761	11.09	0.1127
24	11,437.0	2.72	11.44	0.1101	0.0762	0.0629	0.0394	10.07	0.0629	0.0394	0.0629	0.0394	10.07	0.0629
25	11,439.0	2.71	11.15	0.1393	0.0985	0.0721	0.0458	10.04	0.0721	0.0458	0.0721	0.0458	10.04	0.0721
26	11,440.5	2.69	12.74	0.1786	0.1296	0.1165	0.0788	11.52	0.1165	0.0788	0.1165	0.0788	11.52	0.1165
27	11,452.0	2.70	10.56	0.1175	0.0823	0.0585	0.0366	8.71	0.0585	0.0366	0.0585	0.0366	8.71	0.0585
28	11,473.0	2.66	8.77	0.0786	0.0525	0.0459	0.0283	5.58	0.0459	0.0283	0.0459	0.0283	5.58	0.0459
29	11,495.0	2.72	8.30	0.1106	0.0766	0.0574	0.0366	5.18	0.0574	0.0366	0.0574	0.0366	5.18	0.0574
30	11,516.0	2.69	11.14	0.1989	0.1494	0.1481	0.1052	10.33	0.1481	0.1052	0.1481	0.1052	10.33	0.1481
31	11,519.0	2.69	11.86	0.2610	0.2000	0.1890	0.1390	10.97	0.1890	0.1390	0.1890	0.1390	10.97	0.1890
32	11,521.0	2.69	11.65	0.2332	0.1777	0.1544	0.1103	10.66	0.1544	0.1103	0.1544	0.1103	10.66	0.1544
33	11,523.0	2.68	12.21	0.2240	0.1699	0.1071	0.0729	11.09	0.1071	0.0729	0.1071	0.0729	11.09	0.1071
Confining Pressure 3,775psi														

Permeability versus Porosity @ 500psi



Permeability versus Porosity @ 3,775psi

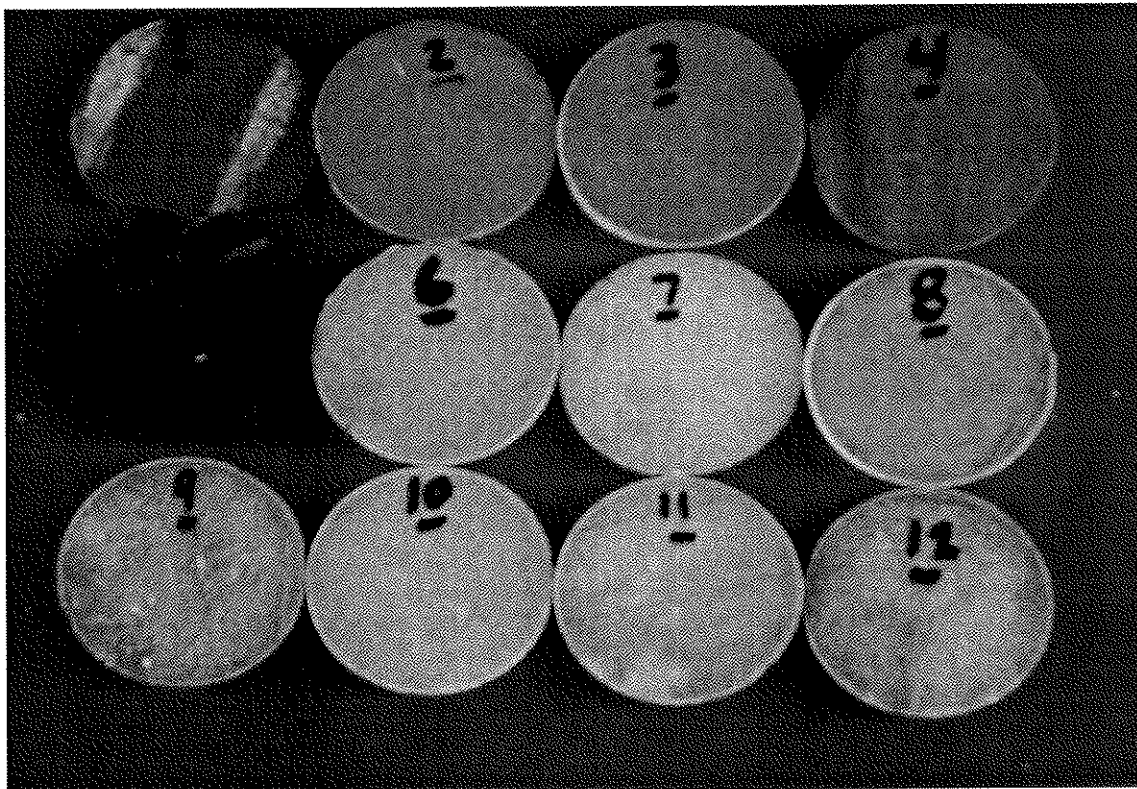
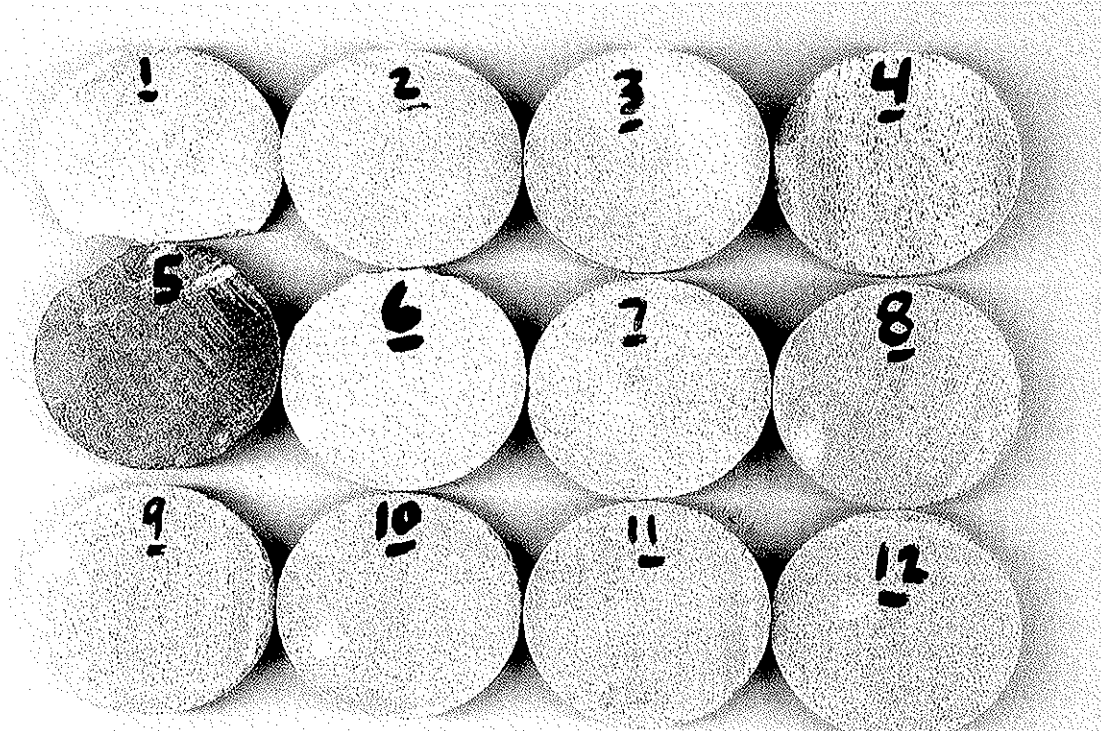




SCAL, Inc.

SPECIAL CORE ANALYSIS LABORATORIES

University 18-41 "A" No. 1-H



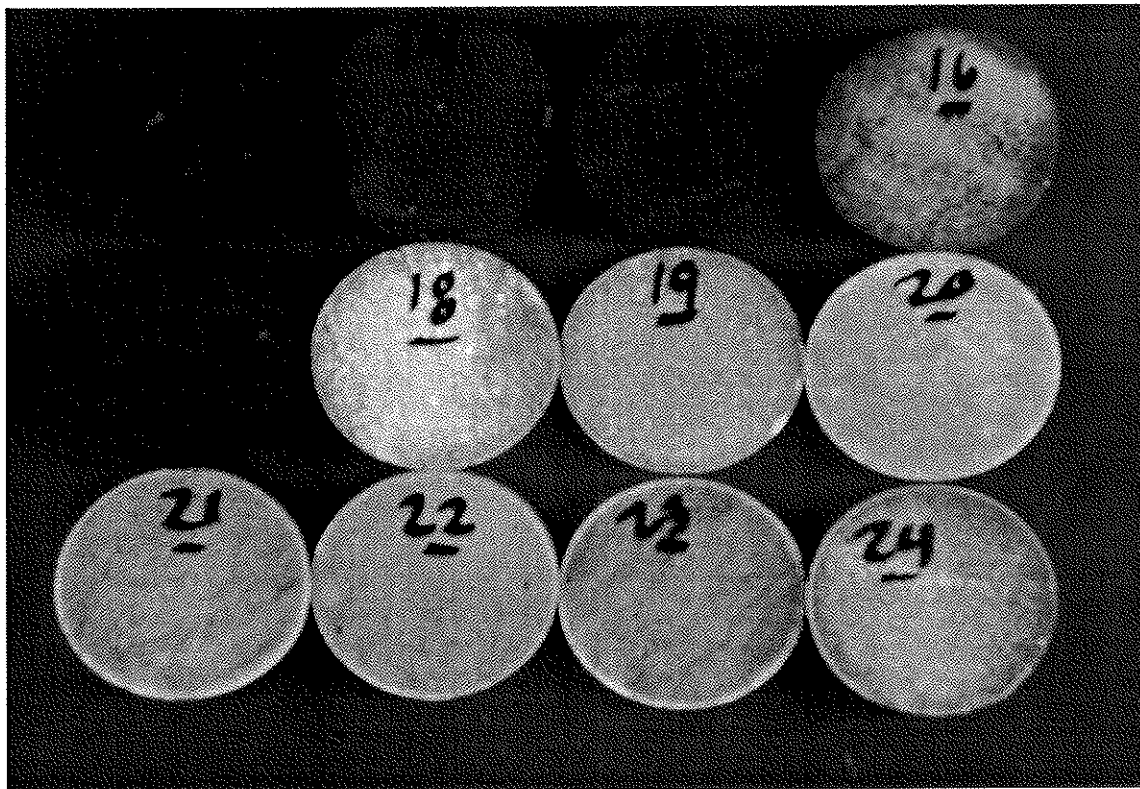
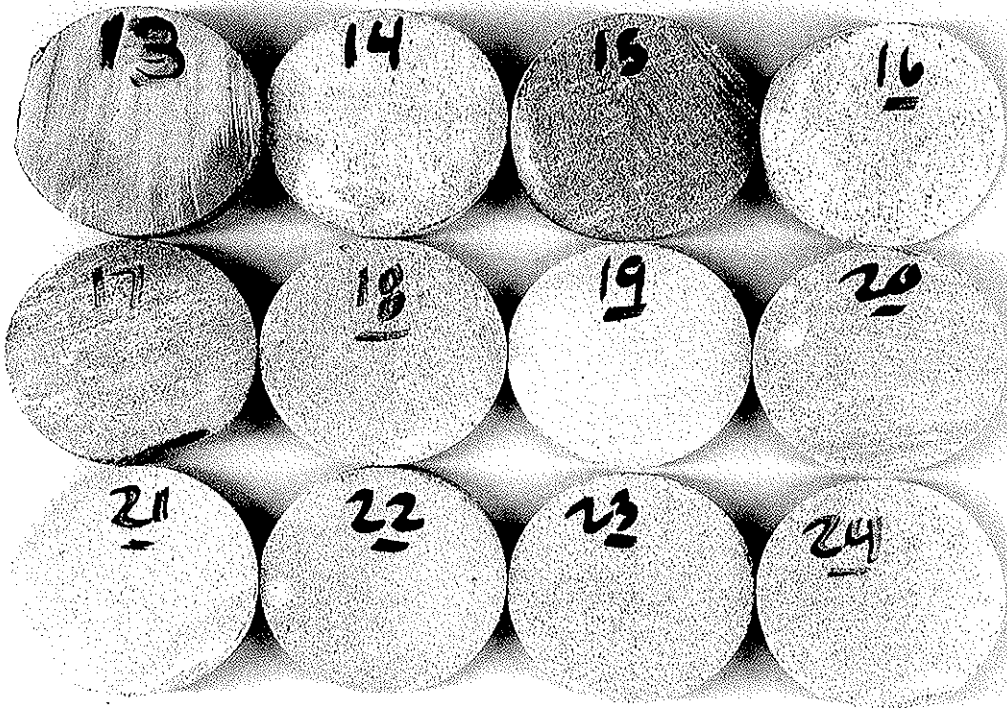
Sample	Depth	Sample	Depth	Sample	Depth	Sample	Depth
1	11,316.0	4	11,327.0	7	11,340.0	10	11,357.0
2	11,318.0	5	11,337.0	8	11,353.0	11	11,359.0
3	11,320.0	6	11,339.0	9	11,355.0	12	11,361.0



SCAL, Inc.

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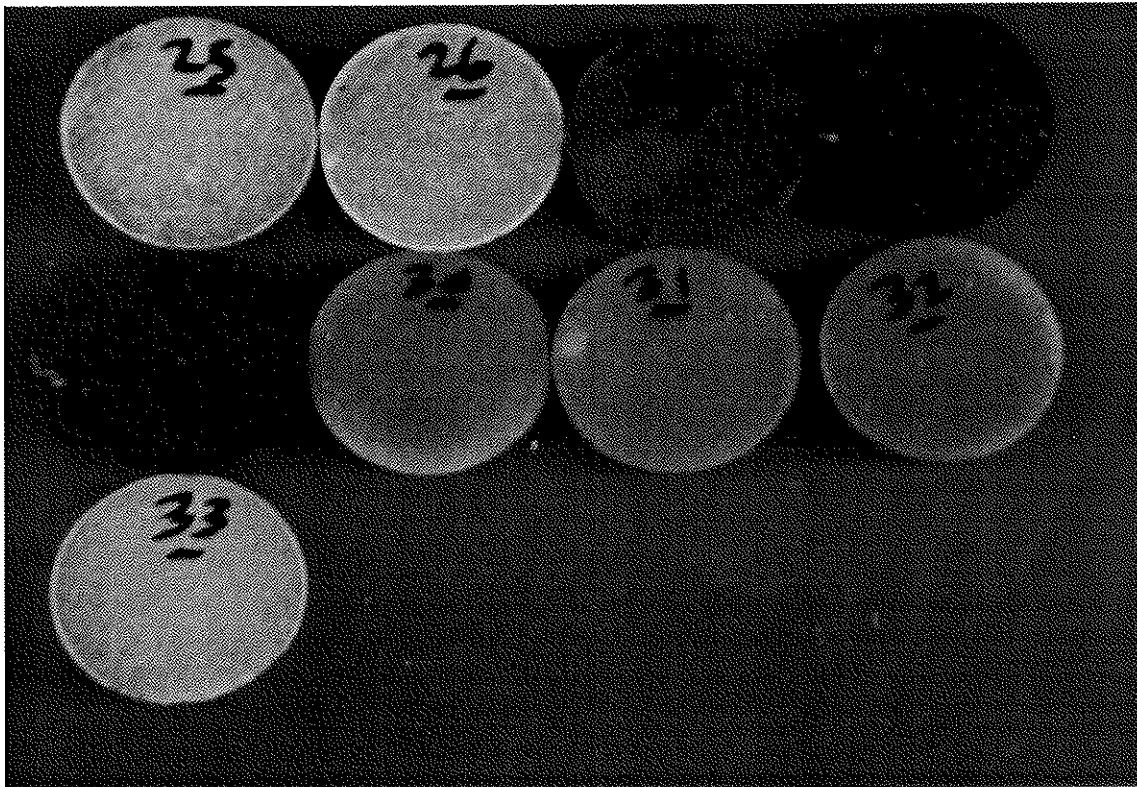
Sample	Depth	Sample	Depth	Sample	Depth	Sample	Depth
13	11,363.0	16	11,406.0	19	11,423.0	22	11,433.0
14	11,381.0	17	11,419.0	20	11,425.0	23	11,435.0
15	11,390.0	18	11,421.0	21	11,431.0	24	11,437.0



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Sample	Depth	Sample	Depth	Sample	Depth
25	11,439.0	28	11,473.0	31	11,519.0
26	11,440.5	29	11,495.0	32	11,521.0
27	11,452.0	30	11,516.0	33	11,523.0